(2

--As battery chargers are typically designed without regard for efficiency, the heat generated via low-efficiency chargers can present a problem. For those applications, the chargers shown in FIGS. 5A-5B delivers 2.5 A with efficiency as high as 96 percent. IC1 is a buck-mode switching regulator that controls the external power switch **Q1** including the synchronous rectifier. IC1 includes a charge pump for thus, generating the positive gate-drive voltage, however required The battery-charging current having a voltage across the 25-M resistor (R3), which is amplified by the op amp and defined, as positive-voltage feedback to IC1. This feedback empowers the chip to maintain the charging current at 2.5 A. While charging, these two circuits H3-H4 can provide current to a separate load, up to a limit, thus set by current-sense transformer T1, and sense resistor R1. T1, thereby improves efficiency by lowering power dissipation in R1. Seeing that the transformer turns ratio (1:70), and routes, only 1/70 of the total battery-plus-load current via R1, generates a feed back voltage, which enables ICl to limit the overall current to a level compatible therewith the external components. As shown in FIG. 4A, a block diagram of a PE model is clear, which was requested via the PTO, such, as to demonstrate its operability. The chargers H3-H4 are connected to each other via the converters V3-V4, whereby two leads proceed from the charger H3, and is connected to the converter V3. While two leads proceed from the charger H4, both leads each of which, consequently, is connected with respect to the converter V4. Seeing that a lead proceeds from the adapter A3, and is connected using the charger jack 2, a lead proceeds from the adapter A4, and is connected by way of the charger jack 3.--

VERSION WITH MARKINGS TO SHOW CHANGES MADE

In the specification:

Paragraph beginning at line 38 of page 3 has been amended as follows:

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FIG. 4 is a perspective view <u>via</u> a bridge <u>with</u> bases on each <u>side</u> of a <u>river</u>, and <u>has</u> <u>two</u> <u>self</u> <u>chargeable</u> <u>batteries</u>;

FIG. 5 is a perspective view of a portion of the bridge adjacent the two battery chargers and their spiraled lights;

Paragraph beginning at line 8 of page 7 has been amended, as follows: Whereby submitted on 12/27/2001.

As shown in FIGS. 5A-5B, the chargers H3-H4 produces current by a controller IC1, a power switch Q1 and a rectifier Q2.

A transformer T1 saves power about Q1's current through R1, as current of an amplifier IC2 flows internally from Rs+to RS- and through R2 to generate a feedback signal for IC1. As shown in FIG. 4A, a block diagram of a model is provided, which was requested via the PTO, such, as to demonstrate its operability. The chargers H3-H4 are connected to each other via the converters V3-V4, whereby two leads proceed from the charger H3, and is connected to the converter V3. While two leads proceed from the charger H4, both leads each of which, consequently, is connected with respect to the converter V4.

Seeing that a lead proceeds from the adapter ${\bf A3}$, and is connected using the charger jack ${\bf 2}$, a lead proceeds from the adapter ${\bf A4}$, and is connected by way of the charger jack ${\bf 3.--}$

Paragraph beginning at line 8 of page 7 has been amended, as follows: Whereby submitted on 03/21/2002.

-As shown via FIGS. 5A-5B, both chargers H3-H4 produces current by a controller IC1, one power switch Q1 and a synchronous rectifier. While charging, these chargers H3-H4 can supply current to any separate load up to a limit set by current-sense transformer T1, and sense resistor R1. T1 improves efficiency by lowering power dissipation in R1, i.e., turning ratio (1:70) via the total battery-plus-load current